



NLC structure electrodynamics design and test results.

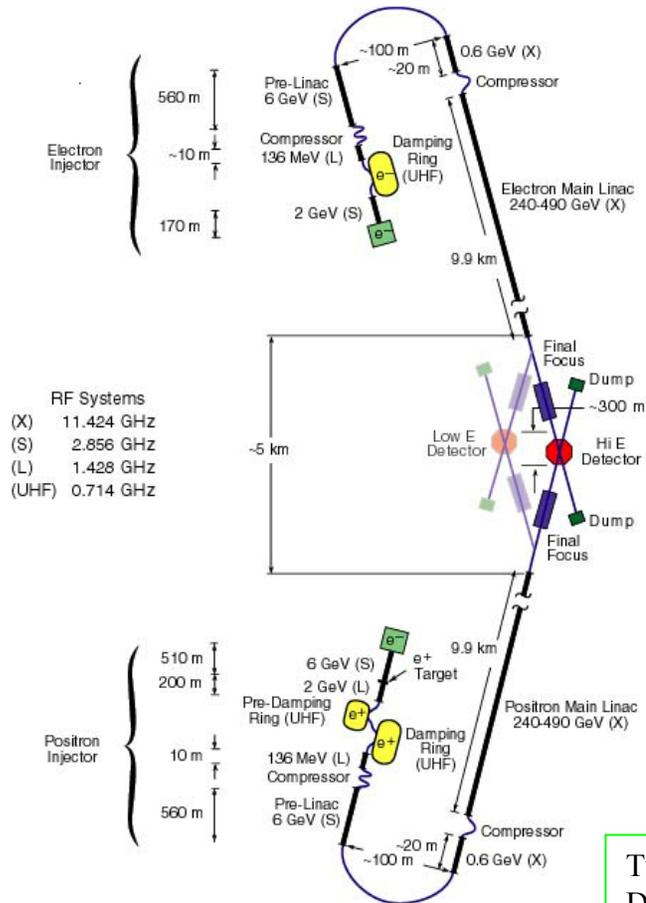
July 11, 2003

G.Romanov



JLC - NLC Accelerator Physics

Next Linear Collider



Two Purposes in support of LC R&D:

- build and demonstrate the technical feasibility of multiple structures (same as converge on a “final” design)
- develop the route to mass-produced structures along with determining their final cost.

• Seven Elements of the RF Factory

- RF Design *
- Produce Copper / Machine Copper *
- RF Measurements & Development / Low Power *
- Structure and Vacuum *
- Mechanical Measurements of Straightness *
- Brazing / Bonding Facility *
- High Power Processing

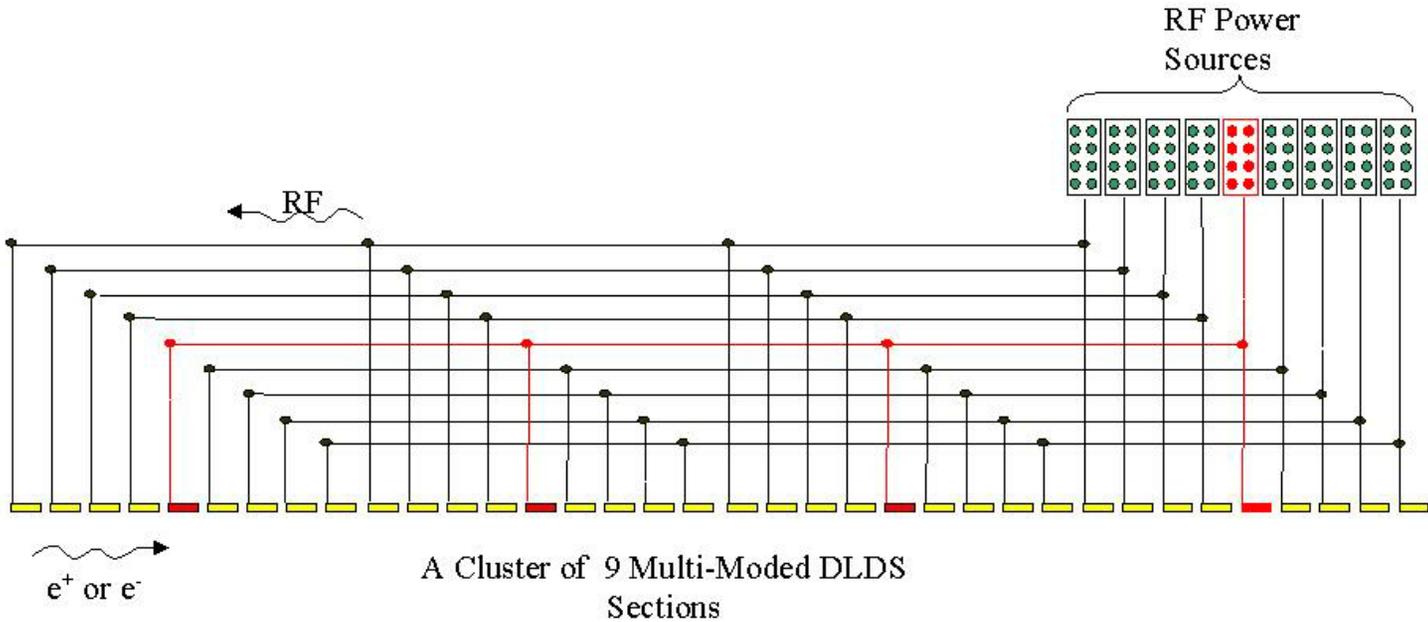
From David Finley’s Presentation at the May 31, 2000 NLC Collaboration Meeting at Fermilab

Tug Arkan, Marco Battistony, Cristian Boffo, Evgeny Borissov, Harry Carter, David Finley, Ivan Gonin, Timergali Khabiboulline, Gennady Romanov, Nikolay Solyak



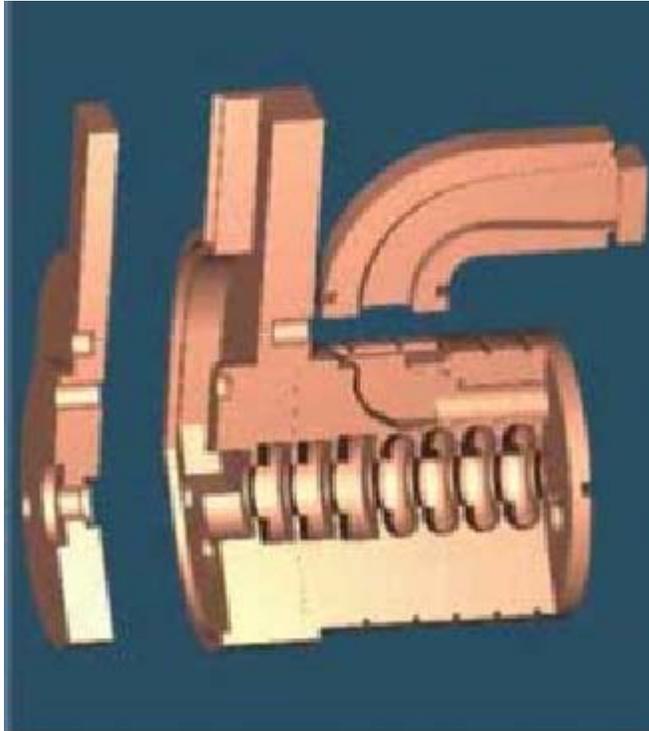
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Next Linear Collider



A Single Multi-Moded Delay Line RF Distribution System

Traveling wave constant gradient detuned damped accelerating structure

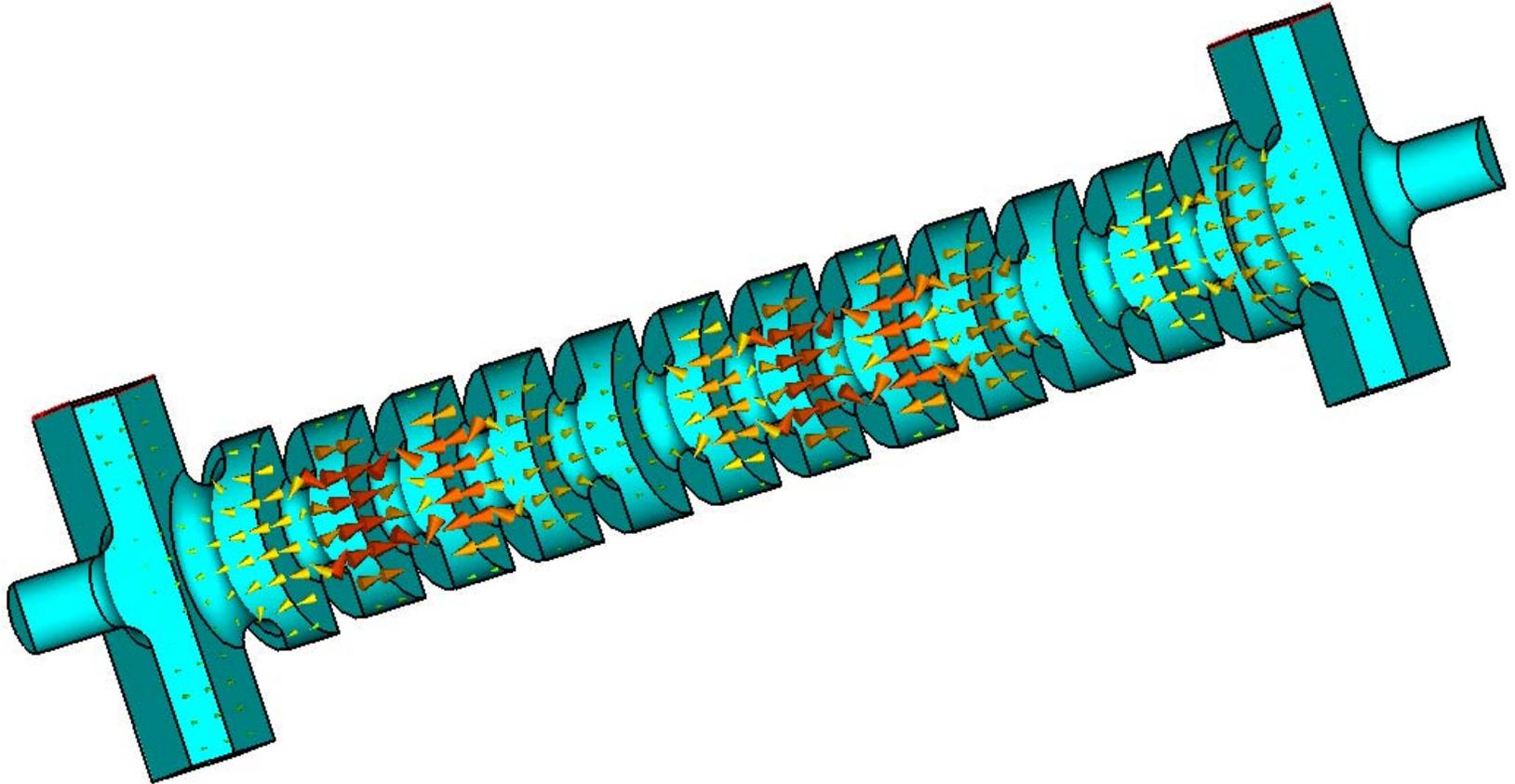


RDDS1

Description: 1.8 m long Rounded, Damped-detuned Structure (RDDS) used in the NLC X-band linacs. "Y" style input rf coupler; double horizontally symmetric output couplers each terminating in water cooled high power rf loads. Internal and external HOM loads. **Average unloaded gradient of 72.3 MV/m**, effective loaded gradient of 55 MV/m. A diffusion brazed assembly of 206, longitudinally coupled copper cells 60 mm OD and 8.75 mm thick which are precision machined to micron tolerances. Integral to the assembly are rf bpm feedthrus brazed to the HOM manifolds. Vacuum pumping is symmetric to both sides of the structure to stabilize vacuum loads.

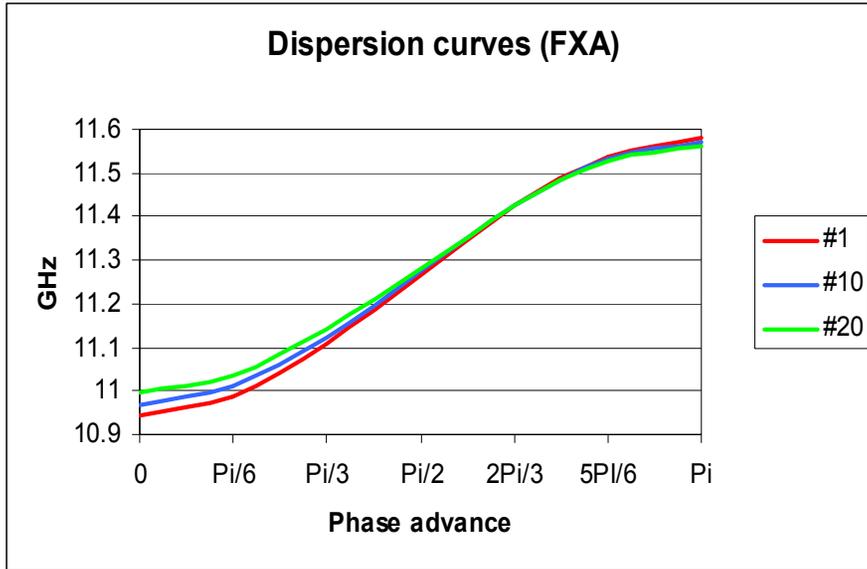
note(1): <3 breakdowns/hr at operating gradients

In spite of all parameter variations, it's still
...traveling wave...



FXB type, 150° phase advance, FNAL waveguide couplers,

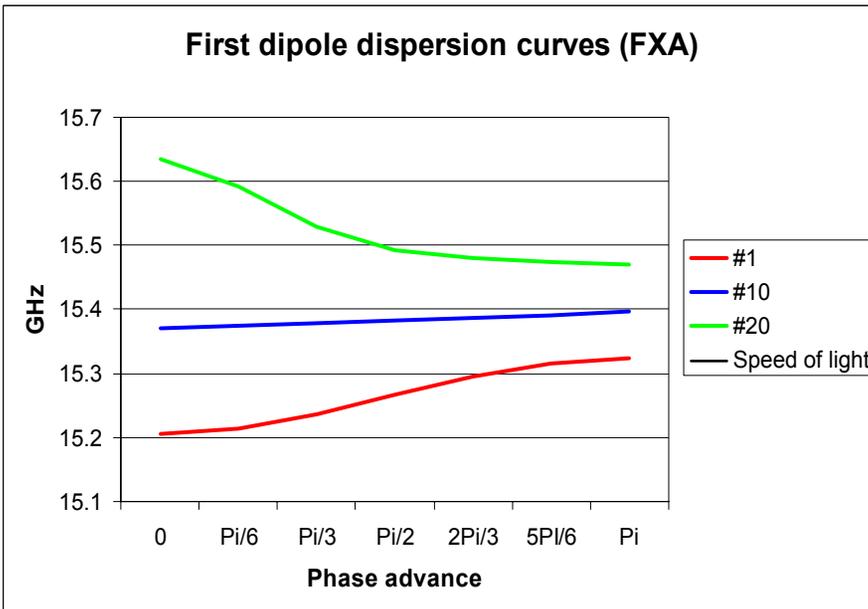
...constant gradient detuned...



R.H.Helm, G.A.Loew. 1969.

“By suitable variation of the transverse modular dimensions, it is feasible to design an accelerator in which the axial electric field are essentially constant along the length of the structure.”

+

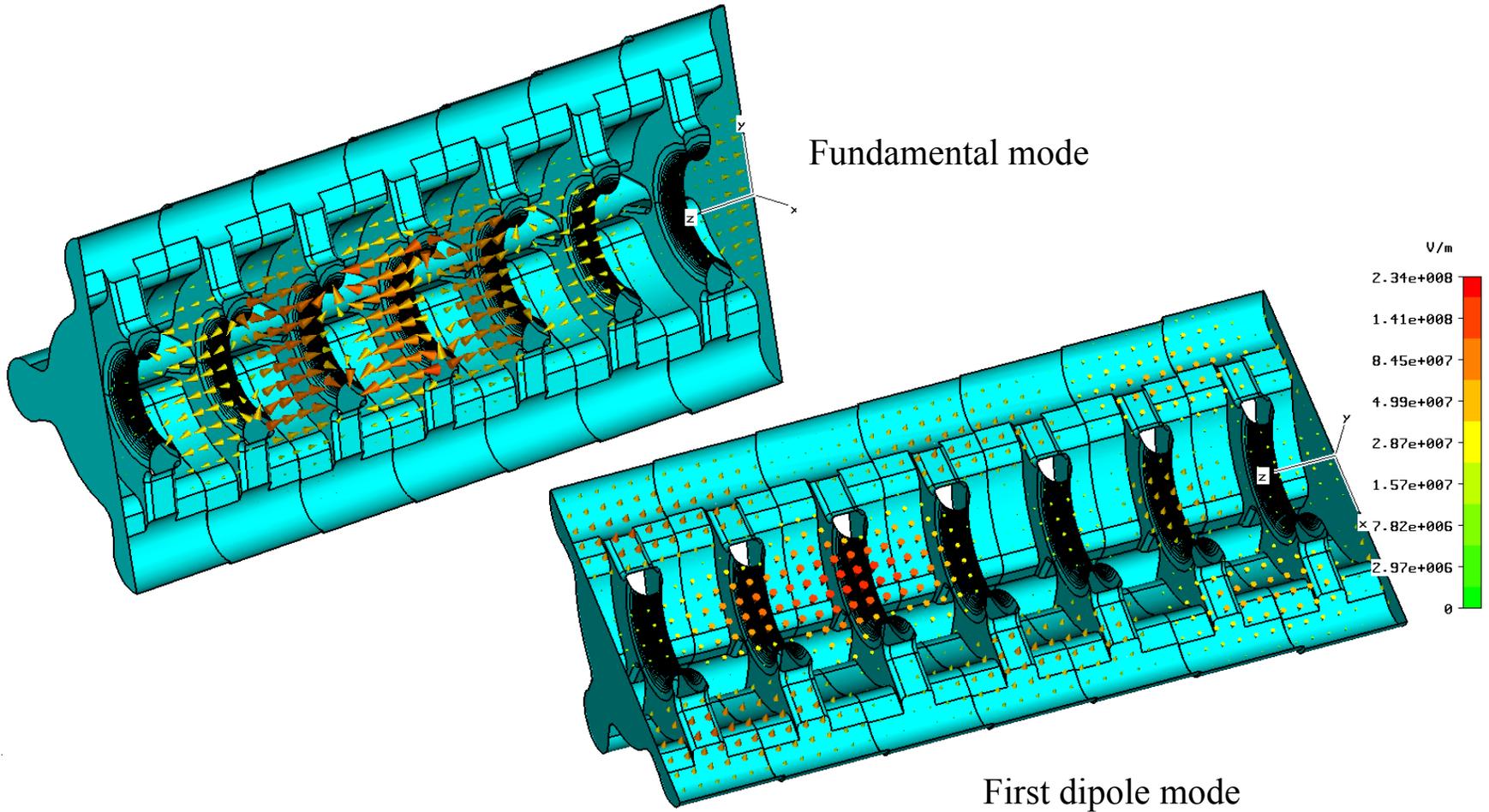


“Another remedy is to displace the \diamond - $\delta\Omega$ of the HEM mode by modifying the modular dimensions of the cavities or perturbing their symmetries ...”

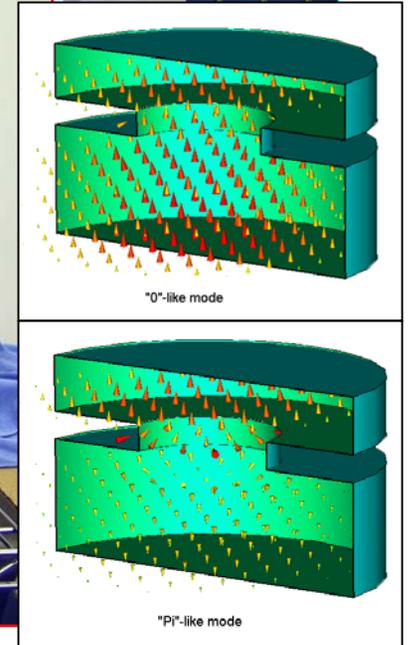
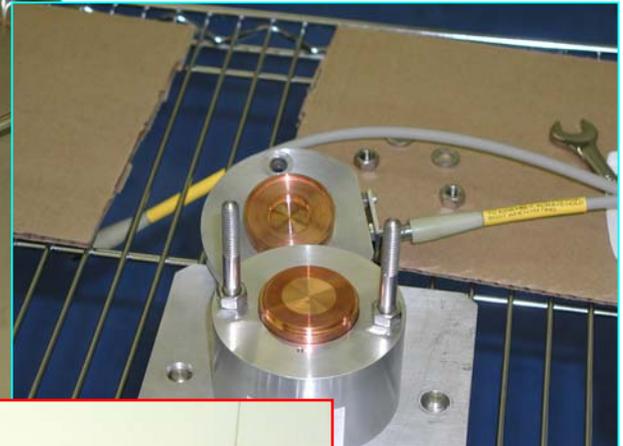
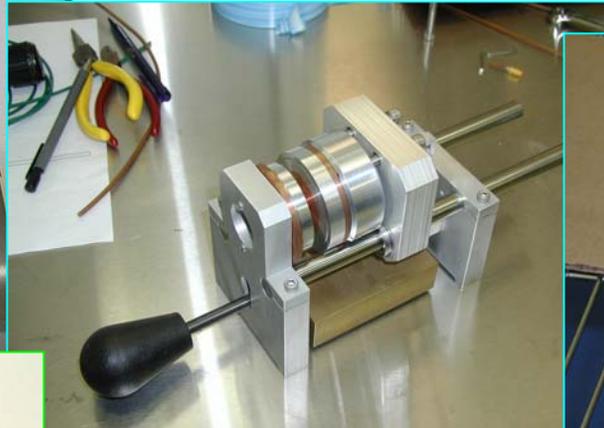
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All disks are different.

...damped accelerating structure.



Single disk QC Set-Up



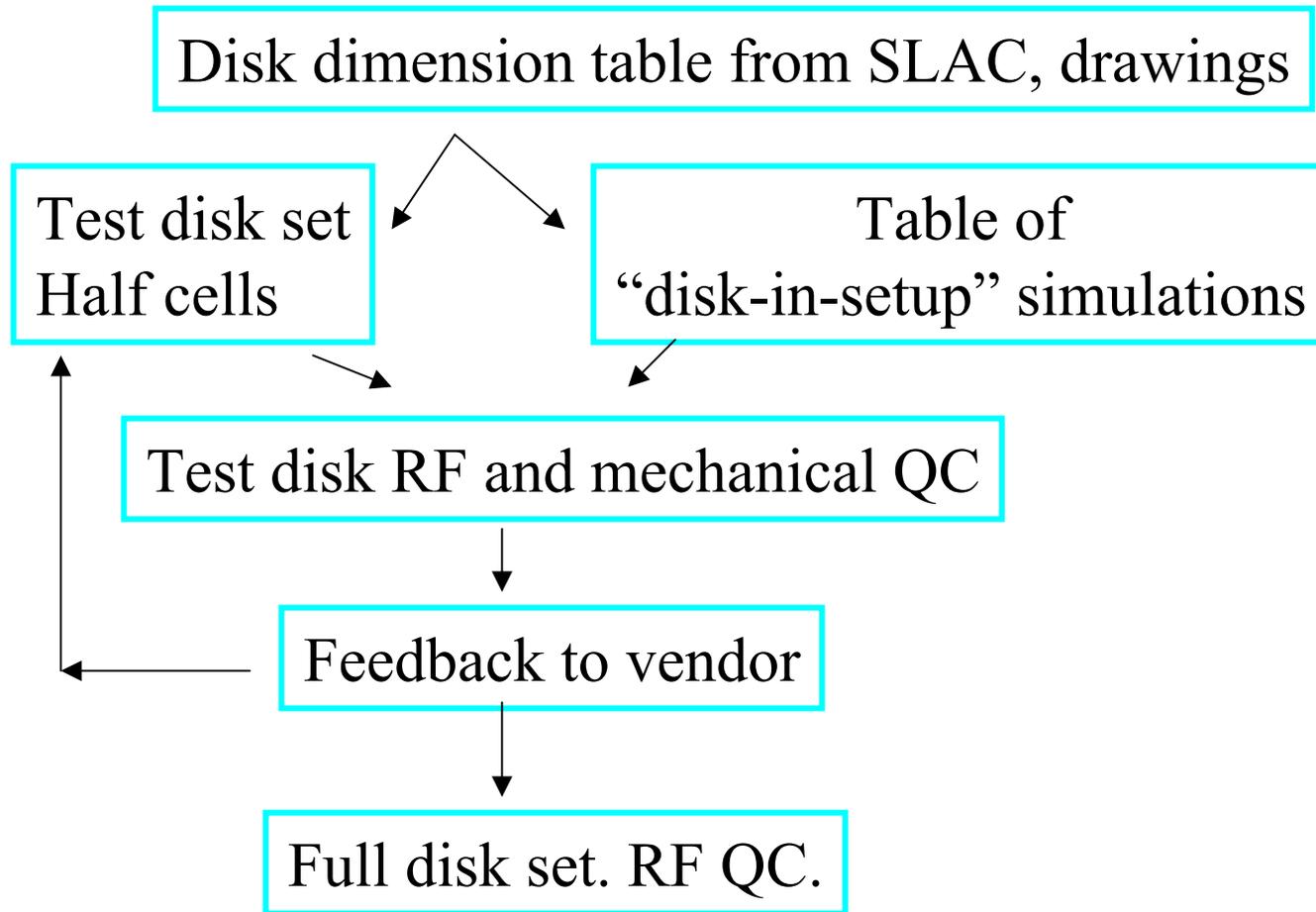
± 0.2 MHz

Not more than ± 0.5 MHz
(goal)

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Single disk QC Set-Up

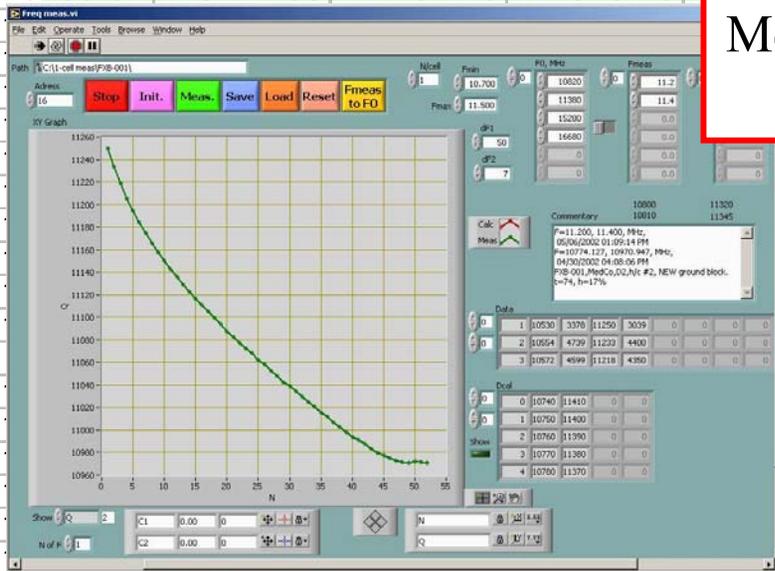




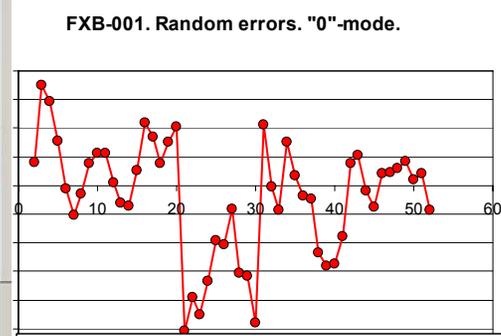
Single disk QC. Automation.

5375.93	4066.513	16721.56	4770.846
5286.43	4092.262	16675.09	4955.865
5286.53	4097.266	16681.53	4955.855

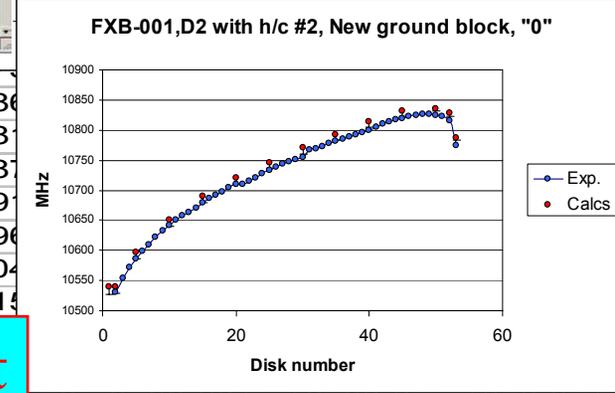
More than 600 measurements of frequency per set



9.95	1516.353	16686.55	1271.711
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6.659
2.851
9.417
5.589
2.921
5.343
254.1
2.476
28.65
9.895



Arbitrary number of modes

On-line control

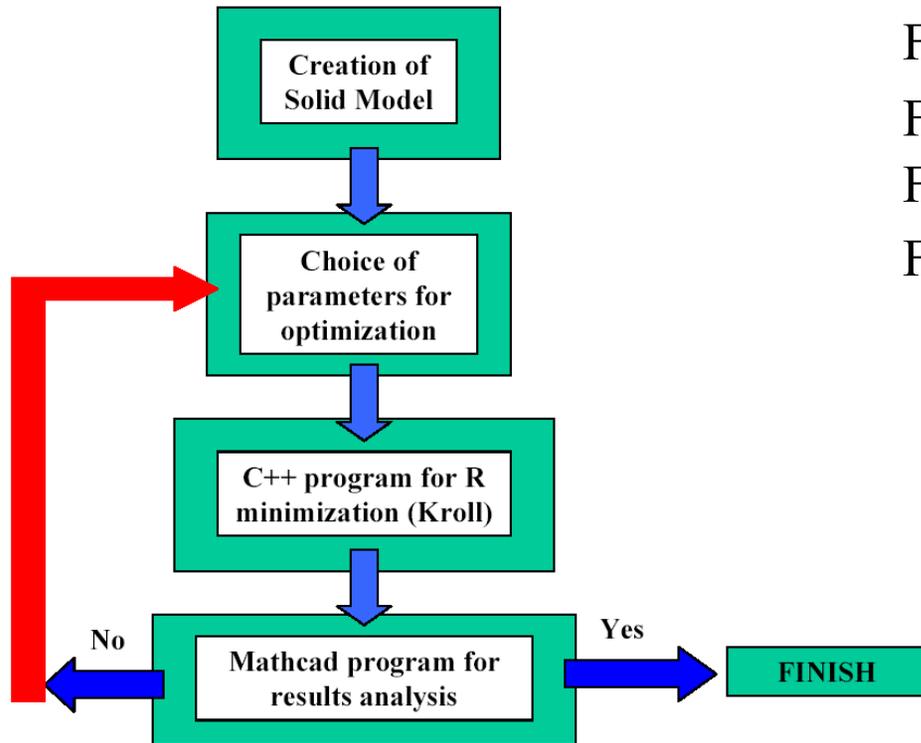
Record is 35 seconds per disk

It's fast

21	10826.68	2053.331	11332.09	1354.798	1507.133
22	10827.00	2053.331	11332.09	1376.345	1538.680
23	10827.32	2053.331	11332.09	1376.345	1538.680
24	10827.64	2053.331	11332.09	1376.345	1538.680
25	10827.96	2053.331	11332.09	1376.345	1538.680
26	10828.28	2053.331	11332.09	1376.345	1538.680
27	10828.60	2053.331	11332.09	1376.345	1538.680
28	10828.92	2053.331	11332.09	1376.345	1538.680
29	10829.24	2053.331	11332.09	1376.345	1538.680
30	10829.56	2053.331	11332.09	1376.345	1538.680
31	10829.88	2053.331	11332.09	1376.345	1538.680
32	10830.20	2053.331	11332.09	1376.345	1538.680
33	10830.52	2053.331	11332.09	1376.345	1538.680
34	10830.84	2053.331	11332.09	1376.345	1538.680
35	10831.16	2053.331	11332.09	1376.345	1538.680
36	10831.48	2053.331	11332.09	1376.345	1538.680
37	10831.80	2053.331	11332.09	1376.345	1538.680
38	10832.12	2053.331	11332.09	1376.345	1538.680
39	10832.44	2053.331	11332.09	1376.345	1538.680
40	10832.76	2053.331	11332.09	1376.345	1538.680
41	10833.08	2053.331	11332.09	1376.345	1538.680
42	10833.40	2053.331	11332.09	1376.345	1538.680
43	10833.72	2053.331	11332.09	1376.345	1538.680
44	10834.04	2053.331	11332.09	1376.345	1538.680
45	10834.36	2053.331	11332.09	1376.345	1538.680
46	10834.68	2053.331	11332.09	1376.345	1538.680
47	10835.00	2053.331	11332.09	1376.345	1538.680
48	10835.32	2053.331	11332.09	1376.345	1538.680
49	10835.64	2053.331	11332.09	1376.345	1538.680
50	10835.96	2053.331	11332.09	1376.345	1538.680
51	10836.28	2053.331	11332.09	1376.345	1538.680
52	10836.60	2053.331	11332.09	1376.345	1538.680
53	10836.92	2053.331	11332.09	1376.345	1538.680
54	10837.24	2053.331	11332.09	1376.345	1538.680
55	10837.56	2053.331	11332.09	1376.345	1538.680
56	10837.88	2053.331	11332.09	1376.345	1538.680
57	10838.20	2053.331	11332.09	1376.345	1538.680
58	10838.52	2053.331	11332.09	1376.345	1538.680
59	10838.84	2053.331	11332.09	1376.345	1538.680
60	10839.16	2053.331	11332.09	1376.345	1538.680

Fundamental mode coupler design

Procedure of couplers optimization



FXA – correction

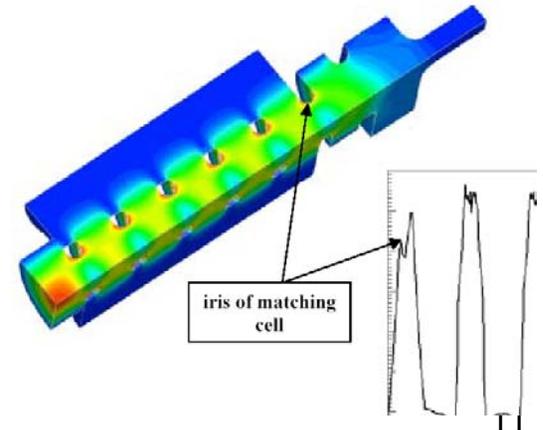
FXB(2,3) – “fat lip”

FXB(4-6) – “waveguide”

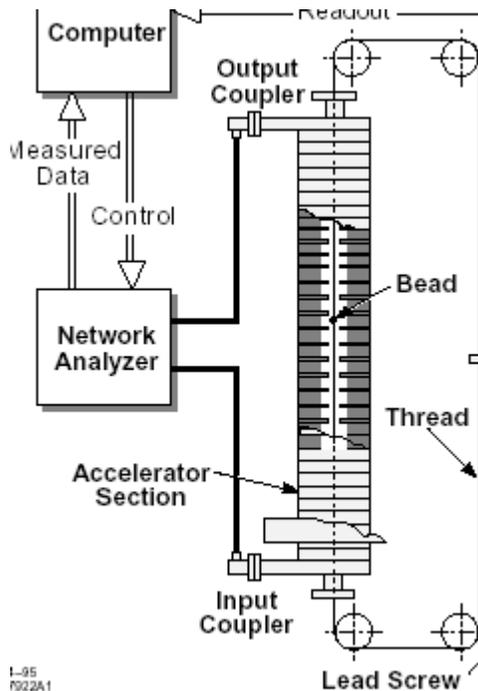
FXC (75 cm, 3D) – “waveguide”

FXC (60 cm) – “waveguide”

FXD(?) – “waveguide”



Structure tuning. Bead-pull.



L-95
F022A1

The traveling wave field distribution measurement is based on a non-resonant perturbation theory [3]. In this technique the measurements of the reflection coefficient S_{11} are measured at the same frequency with and without a perturbing object placed at the point at which the field parameters have to be determined. On the axes of the section the magnetic component of the field is zero and the dependence of the reflection coefficient from the electric component of the field is expressed by the following formula:

$$2P_i (S_{11p} - S_{11a}) = -j\omega k E_a^2 \quad 2.1$$

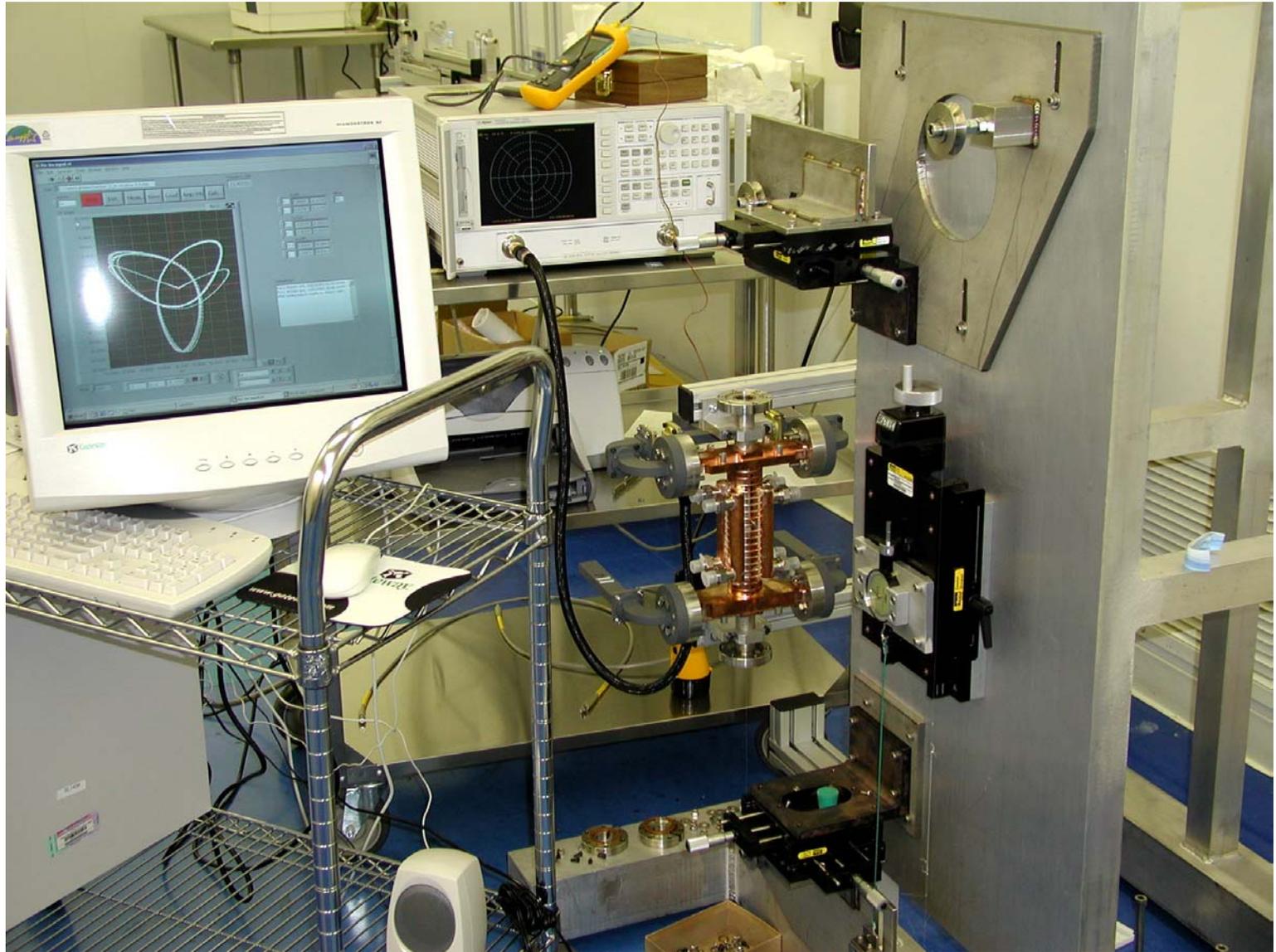
with P_i - the input power, S_{11p} - the reflection coefficient in the presence of a perturbing object, S_{11a} - the reflection coefficient in the absence of the perturbing object, k depends on the electric parameters and the geometry of the object and $E_a = A e^{j\varphi}$ - the electric component of the field. The perturbing

A NEW TUNING METHOD FOR TRAVELING WAVE STRUCTURES

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[3] C.W.Steele, 1966

Structure tuning. Bead-pull



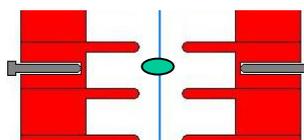
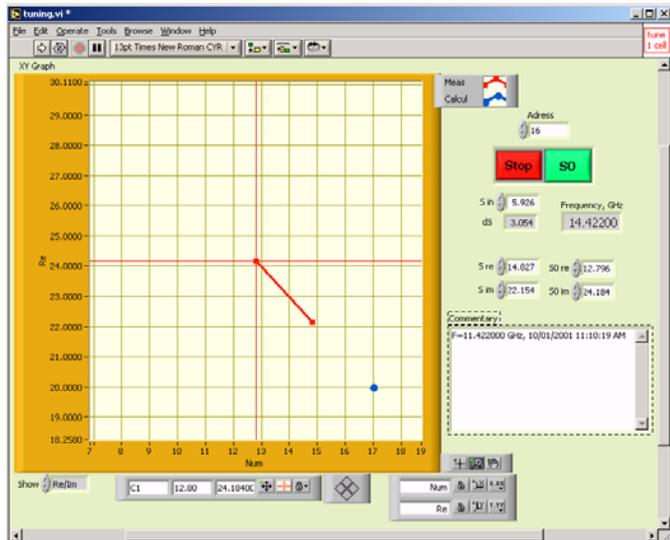
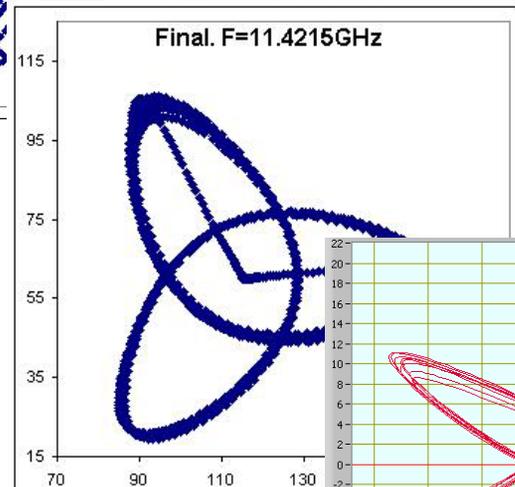
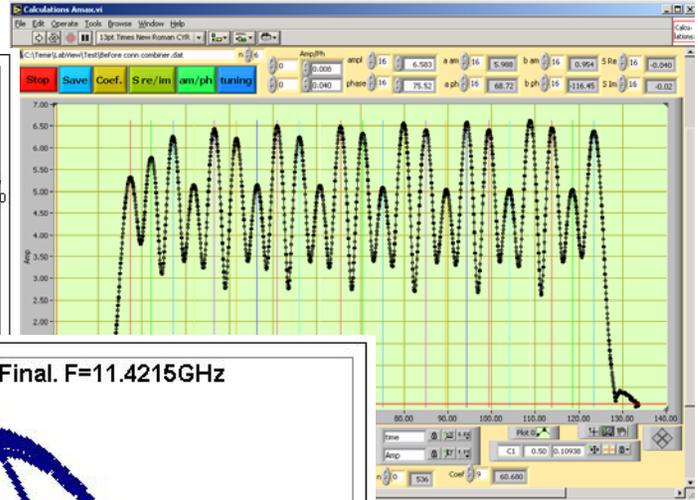
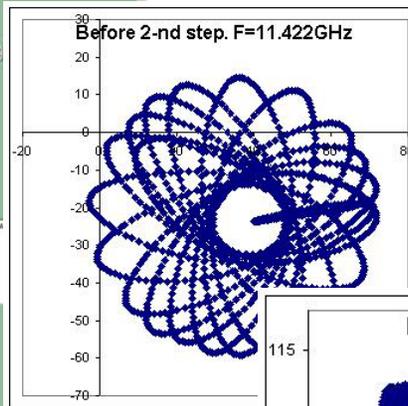
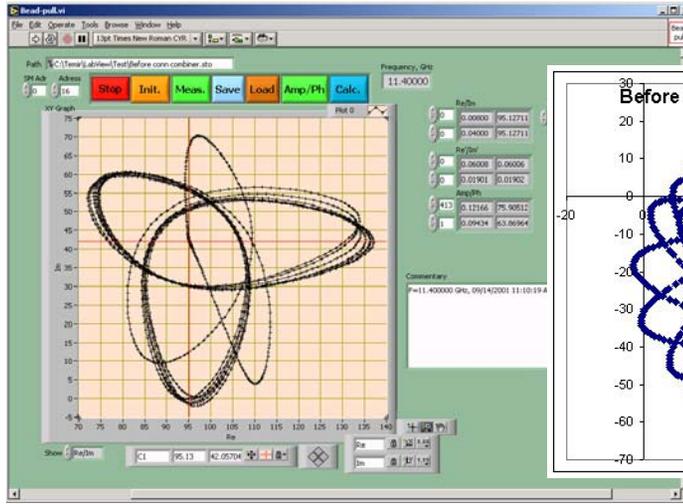
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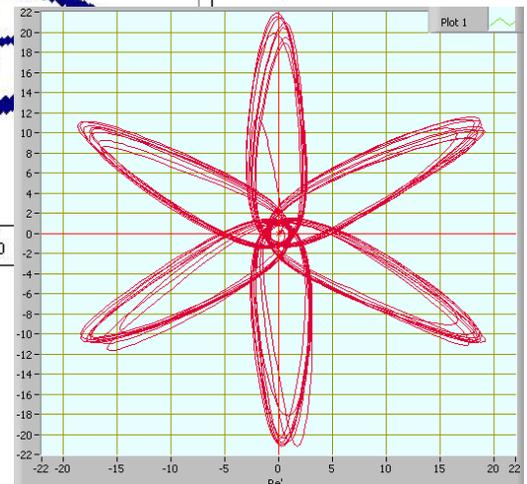
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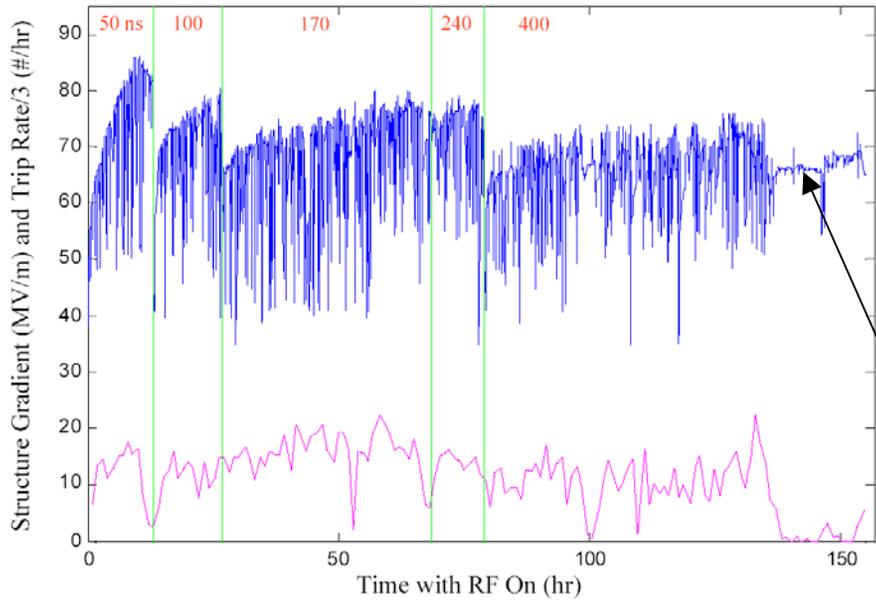
Bead-pull measurements



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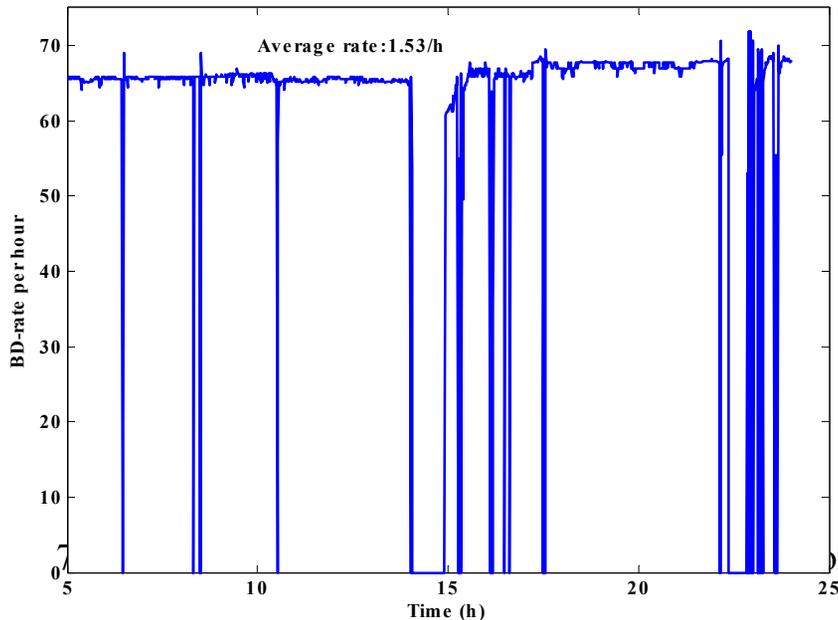
H60VG3_FXB3 Processing History



Short 50nsec pulse processing, 12 hours
 100nsec pulse processing, 12 hours
 170nsec pulse processing, 40 hours
 240nsec pulse processing, 10 hours
 400nsec pulse processing, 60 hours
 400nsec pulse at design accelerating field 65 MV/m, 12 hours

400 ns , first 65 MV/m run. About 1 Breakdowns/h

FXB-003



Later:
 400nsec pulse at design accelerating field 65 MV/m, 8 hours. About 0.6 Breakdowns/h.
 400nsec pulse at accelerating field 67 MV/m, 9 hours. About 2.5 Breakdowns/h.

NLC project:
 400nsec pulse at design accelerating field 65 MV/m. 0.1 Breakdowns/h.

Rumor: Breakdown level 0.25-0.3 per hour for RF pulse 400 nsec and 65 MV/m unloaded accelerating gradient.